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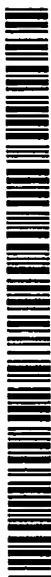


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- (71) Applicant (for all designated States except US): **SHOWA DENKO K. K.** [JP/JP]; 13-9, Shiba Daimon 1-chome, Minato-ku, Tokyo 105-8518 (JP).
- (72) Inventors; and
- (75) Inventors/Applicants (for US only): **OHNO, Hiromoto** [JP/JP]; C/O KAWASAKI PLANT, SHOWA DENKO K. K., 5-1, Ogimachi, Kawasaki-ku, Kawasaki-shi, Kanagawa 210-0867 (JP). **OHI, Toshio** [JP/JP]; C/O KAWASAKI PLANT, SHOWA DENKO K. K., 5-1, Ogimachi, Kawasaki-ku, Kawasaki-shi, Kanagawa 210-0867 (JP).
- (74) Agents: **ISHIDA, Takashi** et al.; A. AOKI, ISHIDA & ASSOCIATES, Toranomon 37 Mori Building, 5-1, Toranomon 3-chome, Minato-ku, Tokyo 105-8423 (JP).
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WO 01/85603 A2

(54) Title: PROCESS FOR PRODUCING NITROGEN TRIFLUORIDE AND USE THEREOF

(57) Abstract: F₂ gas is reacted with NH₃ gas in a gaseous phase at 80°C or less in the presence of a diluting gas to produce NF₃. Thus, NF₃ is produced with good safety, efficiency and profitability.

DESCRIPTION

PROCESS FOR PRODUCING NITROGEN TRIFLUORIDE
AND USE THEREOF

5

Cross-Reference to Related Application

This application is an application filed under 35 U.S.C. § 111(a) claiming benefit pursuant to 35 U.S.C. § 119(e)(1) of the filing date of the Provisional Application 60/230,792 filed September 7, 2000, pursuant to 35 § 111(b).

Technical Field

The present invention relates to a process for producing nitrogen trifluoride (hereinafter it may be referred to as "NF₃"), comprising directly reacting fluorine gas (F₂) with ammonia gas (NH₃) in a gaseous phase and the use thereof.

Background Art

NF₃ is used as a dry etching gas or the like in, for example, the production of semiconductor devices and, in general, the processes for producing NF₃ are roughly classified into chemical processes and electrolytic processes.

Known examples of chemical processes include:

- (1) a method of blowing F₂ gas and NH₃ gas into fused acidic ammonium fluoride (see, Japanese Examined Patent Publication No. 55-8926, JP-B-55-8926),
- (2) a method of reacting a metal fluoride ammonium complex in a solid form with F₂ gas (see, Japanese Examined Patent Publication No. 60-71503, JP-B-60-71503), and
- (3) a method of directly reacting F₂ gas with NH₃ gas (see, Japanese Unexamined Patent Publication No. 2-255513, JP-A-2-255513).

On the other hand, known examples of the electrolytic process using fused acidic ammonium fluoride as an electrolyte include:

(4) a method of performing electrolysis using graphite as an anode, and

(5) a method of performing electrolysis using nickel as an anode.

5 In addition, Ruff et al. have reported that, using the chemical process of reacting F_2 with NH_3 in a gaseous phase, NF_3 can be synthesized, though the yield is as low as 5% or less (see, Z. anorg. allg. Chem., 197, 395 (1931)). Also, Morrow et al. have reported that NF_3 was
10 synthesized similarly in a gaseous phase (see, J. Amer. Chem. Soc., 82, 5301 (1960)).

However, in the conventional direct fluorination process of synthesizing NF_3 from NH_3 as the reaction substrate using F_2 gas, the F_2 gas used is very highly
15 reactive, therefore, explosion or corrosion may occur between the substrate and F_2 gas. Furthermore, these reactions incur generation of a large amount of heat of reaction to increase the temperature in the reactor, as a result, the yield disadvantageously decreases due to
20 decomposition of the product NF_3 or due to the generation of N_2 , HF or NH_4F by the side reactions. The method described in JP-A-2-255513 has a problem in that NF_3 is produced using F_2 gas in 3 to 20 times based on NH_3 , where the reactor temperature is kept at 80 to 250°C
25 within a heat medium, therefore, the yield based on the F_2 is low and the profitability is low.

In the direct fluorination method using F_2 gas, heat of reaction of about -110 kcal/mol is generated when one hydrogen in the substrate is displaced by one fluorine.
30 Therefore, in the case of producing NF_3 by reacting F_2 with NH_3 , heat of reaction of about -330 kcal/mol is generated upon displacement of hydrogen with fluorine and this generation of heat readily causes breakage of the N-F bond or explosion and moreover decreases the yield,
35 giving rise to problems in the production.

Disclosure of Invention

The present invention has been made under these

circumstances and the object of the present invention is to provide a process for producing NF_3 with good safety, efficiency and profitability industrially in the direct fluorination method of producing NF_3 by reacting a
5 substrate (NH_3) with F_2 gas.

As a result of extensive investigations to solve the above-described problems, the present inventors have found that, in the process of producing NF_3 by reacting F_2 gas with NH_3 gas, when the reaction is performed at
10 80°C or less in the presence of a diluting gas, NF_3 can be produced with a high yield. The present invention has been accomplished based on this finding.

Thus, the present invention provides a process for producing NF_3 , and a use of the NF_3 obtained, as
15 described in (1) to (13) below.

(1) A process for producing nitrogen trifluoride, comprising reacting fluorine gas with ammonia gas in a gaseous phase, wherein the reaction is performed at 80°C or less in the presence of a diluting gas.
20

(2) The process as described in (1) above, wherein the reaction temperature is 50°C or less.

(3) The process as described in (1) or (2) above, wherein the concentrations of fluorine gas and ammonia gas fed are from 1:1 to 1:2 in terms of the molar ratio.
25

(4) The process as described in any one of (1) to (3) above, wherein fluorine gas and/or ammonia gas is fed in portions.

(5) The process as described in any one of (1) to (4) above, wherein the concentration of fluorine gas fed is 3 mol% or less.
30

(6) The process as described in any one of (1) to (5) above, wherein the concentration of ammonia gas fed is 6 mol% or less.

(7) The process as described in any one of (1) to (6) above, wherein the diluting gas is at least one selected from the group consisting of nitrogen, helium,
35

argon, hexafluoroethane and octafluoropropane.

(8) The process as described in any one of (1) to (7) above, wherein the diluting gas is reused by circulation.

5 (9) The process as described in any one of (1) to (8) above, wherein a step of treating unreacted fluorine gas is provided and, in the step, unreacted fluorine gas is treated with an aqueous alkali solution and/or alumina.

10 (10) The process as described in (9) above, wherein the treatment step is performed at 80°C or less.

(11) A nitrogen trifluoride product comprising the nitrogen trifluoride obtained by the process described in any one of (1) to (10) above.

15 (12) An etching gas comprising the nitrogen trifluoride product described in (11) above.

(13) A cleaning gas comprising the nitrogen trifluoride product described in (11) above.

20 That is, the present invention provides "a process for producing nitrogen trifluoride, comprising reacting fluorine gas with ammonia gas in a gaseous phase, wherein the reaction is performed at 80°C or less in the presence of a diluting gas", "a nitrogen trifluoride product comprising the nitrogen trifluoride obtained by the
25 production process described above", and "an etching gas and a cleaning gas each comprising the nitrogen trifluoride product described above".

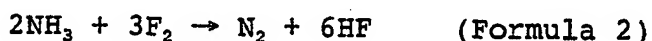
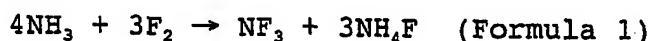
Best Mode for Carrying Out the Invention

The present invention is described in detail below.

30 The present invention provides a process for producing NF_3 by directly (non-catalytically) reacting F_2 gas with NH_3 gas in a gaseous phase at 80°C or less in the presence of a diluting gas, where the problems in conventional direct fluorination reaction techniques can
35 be solved and NF_3 can be industrially produced with good safety, efficiency and profitability.

As described above, the direct fluorination method using F_2 gas incurs generation of heat of reaction as large as about -110 kcal/mol when one hydrogen in the substrate is displaced by one fluorine.

5 In the case of producing NF_3 by reacting F_2 gas with NH_3 gas, a heat of reaction of about -330 kcal/mol is generated only by the displacement of hydrogen by fluorine, and the local temperature increases in many cases. When the temperature is high, a side reaction as
10 shown below by Formula 2 predominantly takes place in addition to the objective reaction as shown below by Formula 1.



15 Accordingly, it is necessary to control the side reaction (Formula 2) and selectively promote the objective reaction (Formula 1). As a result of extensive investigations to solve this problem, the present inventors have found that there is a close relationship
20 between the reaction temperature and the side reaction. If the reaction temperature is 80°C or more, for example, 110°C, the side reaction (Formula 2) predominantly proceeds and only nitrogen and hydrogen fluoride are produced but the objective NF_3 is scarcely produced.
25 When the reaction temperature is lowered to 80°C or less, the objective reaction (Formula 1) selectively proceeds. That is, the reaction temperature in the process of the present invention is 80°C or less, preferably 50°C or less. When the reaction system is further cooled, the
30 objective reaction (Formula 1) proceeds more selectively, however, if the reaction temperature is too low, the reaction rate is also excessively decreased and, depending on the case, the diluting gas may be condensed. Accordingly, the lower limit of the temperature may
35 suitably be -30°C.

For the cooling, a method of circulating the gas using, for example, a jacket system or a coil system may be preferred. Depending on the case, for example, stirring or the like may be used to render the
5 temperature in the reactor uniform. The large heat of reaction is preferably eliminated to prevent a rise in the local temperature.

In order to prevent the local temperature from the rising due to heat of reaction, the starting materials F_2 and NH_3 are preferably fed in portions when the
10 concentrations thereof are high from the standpoint of preventing a rise in the local temperature, though the starting material gases each may be fed in one lot when the concentration thereof is low. In the case of feeding
15 F_2 gas and NH_3 gas as the starting materials in portions, for example, a method of passing F_2 gas and NH_3 gas through a first inlet for feeding starting material gas and passing NH_3 gas through a second inlet for feeding gas may be used. By feeding the gases in portions as
20 such, the reaction temperature can be more effectively prevented from rising locally.

In the direct fluorination reaction using F_2 gas, generation of a large amount of heat accompanies the reaction as described above. For preventing this
25 generation of heat, a method of diluting F_2 gas with an inert gas, a method of diluting NH_3 gas as the substrate with an inert gas and the like may be used. The diluting gas is preferably at least one inert gas selected from the group consisting of nitrogen, helium, argon,
30 hexafluoroethane and octa-fluoropropane. In taking account of the operation of separating and thereby purifying the objective NF_3 (boiling point: $-120^\circ C$) from the inert gas in the distillation process, hexafluoroethane (boiling point: $-78.1^\circ C$) and
35 octafluoropropane (boiling point: $-36.7^\circ C$) each having a high boiling point as compared with NF_3 , are advantageous

in view of the cost for separation. Among these, octafluoropropane is more preferred.

5 In introducing the gases into a reactor, either one or both of F_2 gas and NH_3 gas is preferably diluted with a diluting gas and then introduced into the reactor. In taking account of safety, F_2 gas and NH_3 gas both are preferably diluted with a diluting gas to a lower concentration. The diluting gas separated from the product NF_3 is preferably recovered and used by
10 circulating it. For the recovery of the diluting gas, a distillation separation method may usually be used. For example, in the case of using octafluoropropane as the diluting gas, the objective NF_3 is extracted from the top of the distillation tower as a low boiling fraction and octafluoropropane as the diluting gas is extracted from
15 the bottom of the distillation tower and used by circulating it in the reaction system.

In practicing the reaction of the present invention, the concentrations of both F_2 gas and NH_3 gas fed as the starting materials are preferably in the range of 1:1 to 1:2 in terms of the molar ratio. Even in the case of feeding the starting materials in portions, the ratio of F_2 gas to NH_3 gas used in the whole reaction is preferably within this range. If the molar ratio of NH_3 gas to F_2 gas is more than two times, equipment or the like for recovering unreacted ammonia gas is necessary and this is not profitable, whereas if it is less than one time, unreacted fluorine gas remains in a large amount and this is disadvantageous from the point of view
20 of safety or profitability.

The concentration of F_2 gas fed is preferably 3 mol% or less and the concentration of NH_3 gas fed is preferably 6 mol% or less. Accordingly, the gas composition fed at the reactor inlet preferably contains
35 9 mol% or less of the reaction substrate (F_2+NH_3) and 91 mol% or more of the diluting gas. As described above, in the direct fluorination method using F_2 gas, F_2 gas used

is highly reactive, therefore, NH_3 containing hydrogen may undergo combustion or explosion when exposed to fluorine. Therefore, the important point of the present invention is to prevent the explosion of NH_3 gas and F_2 gas. The present inventors have studied on the range of explosive conditions for NH_3 gas and F_2 gas, as a result, the lower limit of the range of conditions for explosion of NH_3 is found to be 6 mol% or less and from this, the safe range of the reaction in the process of the present invention can be established. Furthermore, by feeding F_2 gas and/or NH_3 gas in portions from two or more gas inlets into the reactor, the gas concentration in the reactor can be controlled to be in a safe range.

Unreacted F_2 gas has a safety problem at the time of concentration or the like in the distillation process and must be removed to the utmost. Therefore, the process for producing NF_3 of the present invention contains a step of treating the unreacted F_2 gas. For removing F_2 gas, a method of contacting the gas with an aqueous alkali solution, for example, an aqueous KOH solution or a method of removing F_2 gas by contacting it with alumina is preferably used. The treating temperature is preferably 80°C or less. If it exceeds 80°C , some of the objective NF_3 may be disadvantageously decomposed.

In the process of producing NF_3 by the direct fluorination reaction of F_2 gas and NH_3 gas, NH_4F is produced as by-product as described above (Formula 1). Therefore, the reaction is preferably performed by employing, for example, a system where two reactor units are used and, by changing over the units, the by-product NH_4F is recovered and reused.

The NF_3 obtained by the production process of the present invention can be used as an etching gas in an etching step during production of a semiconductor device. Also, NF_3 can be used as a cleaning gas in a cleaning step during production of a semiconductor device. In production of a semiconductor device such as an LSI and a

TFT, after forming a thin film or a thick film by CVD, sputtering, evaporation, or the like, etching is performed to form a circuit pattern. Furthermore, in an apparatus for forming a thin film or a thick film, cleaning is performed to remove unnecessary deposits accumulated on the inner wall of the apparatus, a jig and the like. This is performed because unnecessary deposits cause generation of particles. For producing a good quality film, cleaning must be performed on occasion.

The etching using NF_3 may be performed under various dry etching conditions such as plasma etching and microwave etching, and NF_3 can be used by mixing it with an inert gas such as He, N_2 and Ar, or with a gas such as HCl , O_2 and H_2 , in an appropriate proportions.

The present invention is further illustrated below by referring to the Examples and Comparative Examples, however, the present invention is not limited to these examples.

Example 1

An Inconel 600-type reactor having an inside diameter of about 40 mm ϕ and a length of 500 mm (a reactor of a jacket type using a refrigerant circulating cooling system, the reactor being subjected to a passivation treatment with F_2 gas at a temperature of 400°C), was used and the reactor was cooled to 5°C while feeding argon gas at 29.58 Nl/hr (fed in equivalent from each of the NH_3 feeding line and the F_2 feeding line). Thereafter, NH_3 gas and F_2 gas were fed at 0.701 Nl/hr and 0.526 Nl/hr, respectively, to perform the reaction. The NH_3 concentration and the F_2 concentration at the reactor inlet were 2.28 mol% and 1.71 mol%, respectively. Two hours after the initiation of the reaction, the concentrations of hydrogen fluoride and unreacted fluorine gas in the reaction product gas were measured using an aqueous potassium iodide solution and the composition was analyzed by gas chromatography. The

analysis values are shown in Table 1. The yield of NF_3 on an F_2 basis was about 69%. In the Table, "ND" means "not detected".

Table 1

| Reaction Product Gas | Analysis Results |
|-------------------------|------------------|
| Unreacted NH_3 | ND |
| Unreacted F_2 | 0.033 NL/hr |
| NF_3 | 0.121 NL/hr |
| HF | ND |

5

Example 2

A reaction and an analysis were performed under the same conditions and the same operation as in Example 1 except for using an Inconel 600-type reactor having an inside diameter of 40 mm ϕ and a length of 500 mm (a reactor using a heating system by an electric heater; the reactor was subjected to a passivation treatment with F_2 gas at a temperature of 400°C) and changing the reaction temperature to 70°C. The analysis results are shown in Table 2. The yield of NF_3 on an F_2 basis was about 42%.

10

15

Table 2

| Reaction Product Gas | Analysis Results |
|-------------------------|------------------|
| Unreacted NH_3 | ND |
| Unreacted F_2 | 0.112 NL/hr |
| NF_3 | 0.075 NL/hr |
| HF | 0.042 NL/hr |

Comparative Example 1

A reaction and an analysis were performed under the same conditions and the same operation as in Example 1 except for using the same reactor as in Example 2 and changing the reaction temperature to 150°C. The analysis results are shown in Table 3. It was seen that at a high reaction temperature of 80°C or more, NF_3 was not produced at all and only the reaction of Formula 2

20

25

proceeded.

Table 3

| Reaction Product Gas | Analysis Results |
|-------------------------|------------------|
| Unreacted NH_3 | ND |
| Unreacted F_2 | ND |
| NF_3 | ND |
| HF | 0.701 NL/hr |

Example 3

5 A reaction and an analysis were performed under the same conditions and the same operation as in Example 1 except for using an Inconel 600-type reactor having an inside diameter of 40 mm ϕ and a length of 500 mm (a reactor of jacket type using a refrigerant circulating cooling system) and feeding NH_3 in a two-part system of feeding the gas at two positions of the inlet part and the central part of the reactor. The analysis results are shown in Table 4. The yield of NF_3 on an F_2 basis was about 76%.

15

Table 4

| Reaction Product Gas | Analysis Results |
|-------------------------|------------------|
| Unreacted NH_3 | ND |
| Unreacted F_2 | 0.011 NL/hr |
| NF_3 | 0.133 NL/hr |
| HF | ND |

Comparative Example 2

20 A reaction and an analysis was performed under the same conditions and the same operation as in Example 1 except for feeding NH_3 at 0.30 NL/hr, F_2 gas at 1.05 NL/hr and helium gas as a diluting gas at 36.7 NL/hr. The analysis results are shown in Table 5. It was seen that when NH_3 gas was fed in a concentration of one times in mol or less based on 1 mol of F_2 gas, unreacted F_2 gas
25 disadvantageously remained in a large amount.

Table 5

| Reaction Product Gas | Analysis Results |
|-------------------------|------------------|
| Unreacted NH_3 | ND |
| Unreacted F_2 | 0.825 NL/hr |
| NF_3 | 0.049 NL/hr |
| HF | ND |

Comparative Example 3

5 A reaction and an analysis was performed under the same conditions and the same operation as in Example 1 except for feeding NH_3 gas at 1.58 NL/hr, F_2 gas at 0.526 NL/hr and helium gas as a diluting gas at 36.7 NL/hr. The analysis results are shown in Table 6. It was seen that when NH_3 gas was fed in a concentration of
10 two times in mol based on 1 mol of F_2 gas, unreacted NH_3 disadvantageously remained in a large amount.

Table 6

| Reaction Product Gas | Analysis Results |
|-------------------------|------------------|
| Unreacted NH_3 | 0.867 NL/hr |
| Unreacted F_2 | 0.010 NL/hr |
| NF_3 | 0.119 NL/hr |
| HF | ND |

Industrial Applicability

15 As described above, according to the present invention, NF_3 , which was heretofore difficult to produce with a high yield, can be produced with a good yield. Furthermore, the NF_3 produced by the process of the present invention can be used as an etching gas or a
20 cleaning gas.

CLAIMS

1. A process for producing nitrogen trifluoride, comprising reacting fluorine gas with ammonia gas in a gaseous phase, wherein the reaction is performed at 80°C or less in the presence of a diluting gas.
2. The process as claimed in claim 1, wherein the reaction temperature is 50°C or less.
3. The process as claimed in claim 1 or 2, wherein the concentrations of fluorine gas and ammonia gas fed are from 1:1 to 1:2 in terms of the molar ratio.
4. The process as claimed in any one of claims 1 to 3, wherein fluorine gas and/or ammonia gas is fed in portions.
5. The process as claimed in any one of claims 1 to 4, wherein the concentration of fluorine gas fed is 3 mol% or less.
6. The process as claimed in any one of claims 1 to 5, wherein the concentration of ammonia gas fed is 6 mol% or less.
7. The process as claimed in any one of claims 1 to 6, wherein the diluting gas is at least one selected from the group consisting of nitrogen, helium, argon, hexafluoroethane and octafluoropropane.
8. The process as claimed in any one of claims 1 to 7, wherein the diluting gas is reused by circulation.
9. The process as claimed in any one of claims 1 to 8, wherein a step of treating unreacted fluorine gas is provided and in the step, unreacted fluorine gas is treated with an aqueous alkali solution and/or alumina.
10. The process as claimed in claim 9, wherein the treatment step is performed at 80°C or less.
11. A nitrogen trifluoride product comprising the nitrogen trifluoride obtained by the production process described in any one of claims 1 to 10.
12. An etching gas comprising the nitrogen trifluoride product described in claim 11.

13. A cleaning gas comprising the nitrogen trifluoride product described in claim 11.

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- (72) Inventors; and
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- (74) Agents: ISHIDA, Takashi et al.; A. AOKI, ISHIDA & ASSOCIATES, Toranomom 37 Mori Building, 5-1, Toranomom 3-chome, Minato-ku, Tokyo 105-8423 (JP).
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INTERNATIONAL SEARCH REPORT

national Application No
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A. CLASSIFICATION OF SUBJECT MATTER
IPC 7 C01B21/083

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
IPC 7 C01B

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EPO-Internal, PAJ, INSPEC

C. DOCUMENTS CONSIDERED TO BE RELEVANT

| Category * | Citation of document, with indication, where appropriate, of the relevant passages | Relevant to claim No. |
|------------|---|-----------------------|
| A | PATENT ABSTRACTS OF JAPAN vol. 014, no. 582 (C-0792), 26 December 1990 (1990-12-26) & JP 02 255513 A (ASAHI GLASS CO LTD), 16 October 1990 (1990-10-16) cited in the application abstract | 1 |
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☒ Further documents are listed in the continuation of box C.

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Date of the actual completion of the international search

13 February 2002

Date of mailing of the international search report

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Name and mailing address of the ISA

European Patent Office, P.B. 5818 Patentlaan 2
NL - 2280 HV Rijswijk
Tel. (+31-70) 340-2040, Tx. 31 651 epo nl,
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